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3                   APPARATUS AND METHOD FOR SUPPORTING STRUCTURES ON  
4                   OFFSHORE PLATFORMS

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6                   BACKGROUND OF THE INVENTION

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8                 This invention relates to a structure for supporting structures on offshore platforms. More  
9                 particularly, but not by way of limitation, this invention relates to a structure and method for  
10               supporting and compensating for movement during well intervention operations on offshore  
11               platforms.

12               Hydrocarbons are located in subterranean reservoirs. The search for hydrocarbons has  
13               brought operators to remote and exotic areas of the globe. Deep water tracts have been explored  
14               and drilled with increasing frequency in recent years. Platforms set in waters of 1,000 to 2,000  
15               feet have become common place, and in some instances, wells have been drilled in water depths of  
16               over 5,000 feet. Different types of drilling and production platforms have been used in these deep  
17               waters. One type of platform is a tension leg platform (TLP). In the TLP, a floating platform is  
18               connected to the ocean floor via tendons such as steel cables, as is well understood by those of  
19               ordinary skill in the art. Another type of structure used in deep water is the spar platform which  
20               generally is a floating cylindrical structure that is anchored to the ocean floor with steel cable  
21               means. Other types of floating platforms are known in the art. In deep water, a fixed leg type of  
22               platform is generally not an option due to the extreme water depths. The exploration, drilling,

1 completion and production in these deep waters is very expensive. For instance, day rental rates  
2 for floatable drilling rigs can cost over \$300,000 per day in some instances.

3 Wave conditions may cause a cyclic buoyant force on these floating platforms based on  
4 the raising, lowering, heaving and pitching of the platform. Moreover, tidal conditions may cause  
5 a variation in platform height and cause similar buoyant forces. The applied forces will in turn  
6 cause motion on the platform and on the work deck of the platform. Additionally, the  
7 subterranean well that is drilled will have a riser extending from the sea floor to the platform. In  
8 other words, a riser extends from the sea floor to the floating platform. As will be understood by  
9 those of ordinary skill in the art, the riser generally does not move in unison with the platform  
10 since the riser is fixed to the sea floor by different attachment means. Also, the riser does not  
11 experience the same buoyant forces as the floating platform.

12 While an operator is in the midst of performing well work, the motion of the platform can  
13 have detrimental effects on the equipment and ongoing operations. For example, a coiled tubing  
14 unit that is rigged-up and running a string of tools into the well could be lifted upward and/or  
15 downward, and/or sideways due to the motion of the platform. This motion could potentially  
16 cause serious damage such as breaking the connection of the coiled tubing to the riser which in  
17 turn could lead to a catastrophic failure. With prior art designs, operators find it necessary to stop  
18 operations and rig down the connection and then reconfigure the equipment.

19 In the course of performing well intervention work on these offshore wells, the operator  
20 must install numerous devices such as coiled tubing injector heads, lubricators, blow out  
21 preventors, etc. As readily understood by those of ordinary skill in the art, numerous operational  
22 problems may be encountered before, during and after the well intervention work. Hence,

1 operators may find it necessary to rig down certain equipment. In the past, and upon experiencing  
2 operational problems, equipment such as the coiled tubing injector head would have to be rigged  
3 down so that the encountered problem could be solved. However, due to the various movements  
4 being experienced by the floating platform, alignment of the equipment is difficult. A significant  
5 amount of time must be spent in rigging up equipment, which equates to significant sums of  
6 money due to the day rates of the rig.

7 Thus, there is a need for a system and method that will allow an operator to move  
8 components of a well intervention string assembly with greater ease and simplicity. There is also  
9 a need to compensate for motion of a floating platform while undergoing well intervention  
10 procedures. These needs, and many other needs, will be met according to the teachings of the  
11 present invention.

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13 SUMMARY OF THE INVENTION

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16 An apparatus for supporting an injector head is disclosed. The apparatus comprises a base  
17 frame mounted to a platform, wherein the base frame has a first bracket and a second bracket  
18 attached thereto. The apparatus further includes an x-axis frame having a first pivot point and a  
19 second pivot point, and wherein the first pivot point is pivotally connected to the first bracket and  
20 the second pivot point is pivotally connected to the second bracket so that the x-axis frame is  
21 movable along an x-axis, and wherein the x-axis frame has a third bracket and a fourth bracket.

22 The apparatus further comprises a z-axis frame having a third pivot point and a fourth

1 pivot point, and wherein the third pivot point is pivotly connected to the third bracket and the  
2 fourth pivot point is pivotly connected to the fourth bracket, and wherein the upper frame is  
3 movable along the z-axis. A sliding frame assembly is operatively positioned within the z-axis  
4 frame, with the sliding frame assembly having a plurality of rods, and wherein the injector head is  
5 operatively connected to the rods.

6 The apparatus further includes a top plate attached to the z-axis frame so that a cavity is  
7 formed, and wherein the sliding frame assembly is contained within the cavity. The apparatus may  
8 further include a motion restriction means for restricting the x-axis frame movement along the x-  
9 axis and the z-axis frame movement along the z-axis. The apparatus may also contain locking  
10 means for locking the sliding frame assembly.

11 In one preferred embodiment, the sliding frame assembly comprises a sliding layer and an  
12 adapter frame. The sliding layer may comprise a fabric so that the fabric slides on the surface of  
13 the z-axis frame. Also, in one preferred embodiment, the injector head is connected to a riser and  
14 wherein the base frame is connected to a floating platform. Also, in one preferred embodiment,  
15 the base frame is mounted on a track stack structure, and the track stack structure is mounted to  
16 the platform.

17 The motion restriction means may comprise an x-axis biasing means for biasing the x-axis  
18 frame along the x-axis, and a z-axis biasing means for biasing the z-axis frame along the z-axis.

19 In one preferred embodiment, the x-axis biasing means comprises a first hydraulic cylinder  
20 attached to the base frame and a first piston extending from the first hydraulic cylinder, and  
21 wherein the first piston is attached to the x-axis frame. In the preferred embodiment, the z-axis  
22 biasing means comprises a second hydraulic cylinder attached to the x-axis frame and a second

1 piston extending from the second hydraulic cylinder, the second piston being attached to the z-  
2 axis frame.

3 A method for compensating for the movement of a floating platform having a riser  
4 extending therefrom is also disclosed. The method comprises providing an apparatus comprising:  
5 a base frame mounted to the platform; a x-axis frame having a first pivot point and a second pivot  
6 point, and wherein the first and second pivot point is pivotly connected to a first and second  
7 bracket on the base frame so that the x-axis frame is movable along an x-axis, and wherein the x-  
8 axis frame has a third bracket and a fourth bracket; a z-axis frame having a third pivot point and a  
9 fourth pivot point, and wherein said third pivot point is pivotly connected to said third bracket and  
10 said fourth pivot point is pivotly connected to the fourth bracket, and wherein the z-axis frame is  
11 movable along the z-axis.

12 The method includes moving the platform due to wave action and pivoting the z-axis  
13 frame about the third and fourth pivot point. The method further includes pivoting the x-axis  
14 frame about the first and second pivot point. In one preferred embodiment, the apparatus has a  
15 sliding frame assembly operatively associated with the z-axis frame, and wherein the method  
16 further comprises moving the sliding frame assembly in a lateral plane in response to the platform  
17 movement. The method may further include restricting the movement of the x-axis frame along  
18 the x-axis, and restricting the movement of the z-axis frame along the z-axis.

19 An advantage of the present invention is that the system and method can be used on  
20 floating platforms. Another advantage is that the system and method provides for motion  
21 compensation on a well undergoing well intervention and remedial well work. Yet another  
22 advantage is that the apparatus can be used with other motion compensation devices such as the

1 apparatus disclosed in U.S. patent application serial number 10/736,267 entitled "Motion  
2 Compensation System and Method", filed 15 December 2003, which is incorporated herein by  
3 express reference. Still yet another advantage is that the present invention allows for performing  
4 coiled tubing well work safely.

5 A feature of the present application is the use of a sliding frame assembly that allows the  
6 lateral movement of an attached structure relative to the apparatus. Another feature is the x-axis  
7 frame that supports an injector head on a floating platform, and wherein the x-axis frame pivots  
8 along the x-axis. Still yet another feature is the z-axis frame that supports an injector head on a  
9 floating platform, and wherein the z-axis frame pivots along the z-axis.

10 Another feature includes the modular design of the components. The modularity allows  
11 for ease of transportation, delivery and rig up. Yet another feature includes the ability to use the  
12 apparatus with a track stack, and wherein the track stack can be used to build the height needed  
13 on specific well applications by simply stacking spacers one on top of the other.

14 Another feature is that motion compensation is provided in the vertical direction and  
15 horizontal direction as well as along the x and z axis. Yet another feature is biasing means that  
16 restricts and controls the amount of pivoting of the z-axis frame and the x-axis frame. Still  
17 another feature is the use of an adapter frame that is part of the apparatus and connects to the  
18 injector head.

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21 BRIEF DESCRIPTION OF THE DRAWINGS

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1           **FIGURE 1A** is an exploded isometric view of the bottom half of the apparatus of the  
2 preferred embodiment of the present invention.

3           **FIGURE 1B** is an exploded isometric view of the top half of the apparatus of the preferred  
4 embodiment of the present invention.

5           **FIGURE 2** is an isometric assembled view of the apparatus of the preferred embodiment  
6 of the present invention seen in FIGURES 1A and 1B.

7           **FIGURE 3** is a cross-sectional view of the isometric illustration of the apparatus taken  
8 along line 3-3 of FIGURE 2.

9           **FIGURE 4** is a schematic illustration of the apparatus of the present invention as part of  
10 the well intervention string assembly on a floating platform.

11          **FIGURE 5** is a schematic illustration of the apparatus seen in FIGURE 4 with a tilt angle  
12 to the port side.

13          **FIGURE 6** is a schematic illustration of the apparatus seen in FIGURE 4 with a tilt angle  
14 to the starboard side.

15          **FIGURE 7** is a schematic illustration of the top view of the apparatus seen in FIGURE 4.

16          **FIGURE 8** is a schematic illustration of the top view of the apparatus seen in FIGURE 4  
17 depicting lateral travel.

18          **FIGURE 9** is a schematic illustration of the motion restriction system of the present  
19 invention.

1                   DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

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3                 Referring now to Fig. 1A, an exploded isometric view of the apparatus 2 of the preferred  
4 embodiment of the present invention will now be described. The apparatus 2 contains a base  
5 frame 4, wherein the base frame 4 is generally rectangular having a first side 6, second side 8,  
6 third side 10, and fourth side 12. In the most preferred embodiment, the sides are of equal length  
7 so that the base frame is a square. The side 8 has a cylinder bracket 14 that will have operatively  
8 associated therewith the cylinder means 16. The side 12 has a cylinder bracket (not seen in this  
9 view) that will have operatively associated therewith the cylinder 18. The base frame 4 will also  
10 contain a first cradle 20 attached to the side 10, and a second cradle 22 attached to the side 6. As  
11 will be explained in greater detail later in the application, the base frame 4 is attached to the deck  
12 of a floating platform, such as a floating drilling rig.

13                 The apparatus 2 further contains an x-axis frame 26 and wherein the x-axis frame 26 is  
14 generally rectangular, having the first side 28, second side 30, third side 32, and fourth side 34.  
15 The side 30 contains the cradle 36, and the side 34 contains the cradle 38. The side 32 contains  
16 the bracket 40 and the side 28 contains a bracket (not seen in this view). The bracket 40 will have  
17 a cylinder means 42 operatively associated therewith, while the other bracket will have cylinder  
18 means 44 operatively associated therewith. The cylinder means 42 has piston 43 extending  
19 therefrom. The x-axis frame 26, in the most preferred embodiment, is a square with the sides  
20 being of equal length. Also, in the most preferred embodiment, the sides of the x-axis frame 26  
21 are longer than the sides of the base frame 4 so that the x-axis frame 26 can fit over the base  
22 frame 4.

1       The x-axis frame 26 further contains a pin 46 and bushing 48 that cooperate with the  
2 opening 50. The bushing 48 will fit into the cradle 20. A pin 51 and bushing 52 cooperate with  
3 the opening 54. The bushing 48 will cooperate with the cradle 20 forming a pivot point and the  
4 bushing 52 will cooperate with the cradle 22 forming a pivot point, which in turn will allow the x-  
5 axis frame 26 to pivot relative to the base frame 4 in the x-axis as seen by arrow A???.

6       The cylinder means 16 will be attached at one end to the side 8, and the piston 56 will be  
7 attached to the side 30 of the x-axis frame 26. Cylinder will also be attached at one end to the  
8 side 12, and the piston 58 will be attached to the side 34 of the x-axis frame 26. In this way, the  
9 cylinder means 16 and 18 are means for restriction for the motion of the x-axis frame 26 in the x-  
10 axis. In the most preferred embodiment, the motion restriction means allows for the tilting of the  
11 x-axis frame 26 in a 2 degree plane in either direction, as will be more fully discussed in the  
12 written description of Figs. 5 and 6.

13       Referring again to Fig. 1A, the z-axis frame 62, which is generally a rectangular frame.  
14 The z-axis frame 62 includes the side 64, side 66, side 68, and side 70. In the most preferred  
15 embodiment, the sides are of equal length thereby making the z-axis frame 62 a square. The side  
16 66 contains an opening 72 that contains the pin 74 and bushing 76 therein. The side 70 contains  
17 an opening and pin (not shown in this view), as well as bushing 78. A bracket 79 is included that  
18 will be connected to the piston 43 as will be described later in the application. The z-axis frame  
19 62 pivots in the z-axis as seen by arrow B.

20       A cover plate 80 attaches the sides of the z-axis frame 62, wherein the cover plate 80  
21 contains an opening 82. The z-axis frame 62 further comprises a lip structure 84, that contains  
22 openings for placement of bolts (not seen in this view), and wherein the lip structure 84, which is

1 in the shape of an inverted L, extends along the sides of the z-axis frame 62.

2 Also seen is the bottom pillow blocks 86 and 88 that is attached to the underside of the  
3 cover 80 that will cooperate with the bushings 48, 52, respectively, in order to keep the z-axis  
4 frame 62 in a stable state. Pillow blocks 89a and 89b are also attached to the underside of cover  
5 plate 80 and will cooperate with bushings 78, 76 in order to keep the z-axis frame 62 in a stable  
6 state.

7 Referring now to Fig. 1B, Fig. 1B also depicts the sliding frame assembly, seen generally at  
8 92. The sliding frame assembly 92 is generally a rectangular frame having side 94, side 96, side 98,  
9 and side 100. In the preferred embodiment, a first strip of elastomer 102 (sometimes referred to as  
10 a sliding pad) is placed on the front sides and a second strip of elastomer 104 (sometimes referred  
11 to as a sliding pad) is placed on the opposite side. The second strip of elastomer 104 will contact  
12 the top face of cover plate 80 (seen in Fig. 1A) so that the sliding frame assembly 92 will slide on  
13 the top face of cover plate 80. Returning to Fig. 1B, the sliding pads 102 and 104 may be  
14 constructed of any material that reduces friction and allows for lateral movement. In the preferred  
15 embodiments, the sliding pads are commercially available from Acadiana Ruber & Gasket Inc.  
16 under the name Nylatron. Other types of materials could be used instead of the elastomer strip  
17 102, such as rubber.

18 The sliding frame assembly 92 further comprises vertically extending rods, wherein the rods  
19 are positioned at each of the corners of the sliding frame assembly 92. Fig. 1 depicts the vertical  
20 rod 110, vertical rod 112, vertical rod 114, and vertical rod 116. The vertical rods 110-116 also  
21 have stop rings, namely stop ring 118, stop ring 120, stop ring 122, and stop ring 123 for the rod  
22 116.

1           Returning to Fig. 1A, a means for locking the sliding frame assembly 92 from movement is  
2 also disclosed. The locking means prevents the sliding frame assembly 92 from moving. This may  
3 be required for some operations wherein it is desirable to keep the sliding frame assembly 92 from  
4 moving, or keeping the sliding frame assembly from shifting when transporting the apparatus 2, for  
5 instance. Also, the locking means can serve as an indexing tool to locate and position the sliding  
6 frame assembly 92. The means for locking comprises horizontal rods 124, 126, 128, 130 disposed  
7 through openings in the sides of the lip structure 84. As shown, the rods contain handles. In one  
8 embodiment, the openings in the sides of the lip structure 84 will contain a threaded block, and the  
9 rods will have mating threads, so that the rods 124-130 can be threaded into and out of the  
10 openings. In this way, the rods 124-130 can be advanced into the cavity and abut the sliding frame  
11 assembly 92 thereby locking the sliding frame assembly 92 in place.

12           Referring again to Fig. 1B, the assembly further comprises a top plate weldment 140,  
13 wherein the top plate weldment 140 will be attached to the lip structure 84 via conventional means  
14 such as nuts and bolts through the openings in the lip structure 84. Other attachment means  
15 includes welding the top plate weldment 120 to the lip structure 84. The top plate weldment 140  
16 contains the corner opening 142, the corner opening 144, the corner opening 146, and the corner  
17 opening 148. The stop rings 118, 120, 122, 123 keep the injector head or the adapter frame above  
18 the openings 142, 144, 146, and 148. The top plate weldment 140 also contains the central  
19 opening 150. The vertical rod 110 will fit through the opening 142, the vertical rod 112 will fit  
20 through opening 144, the vertical rod 114 will fit through opening 146 and the vertical rod 116  
21 will fit through opening 148.

22           Fig. 1B also depicts the adapter frame, seen generally at 154. As understood by those of

1 ordinary skill in the art, the adapter frame 154 will be connected to the injector head (not seen in  
2 this view). The adapter frame 154 is generally rectangular with a first side 156, a second side 158,  
3 a third side 160, and a fourth side 162. At each of the corners, there is contained an opening for  
4 concentric placement of the vertical rods. Hence, the opening 164 is adapted to receive rod 110;  
5 opening 166 is adapted to receive rod 112; opening 168 is adapted to receive rod 114; and opening  
6 170 is adapted to receive rod 116. The adapter frame 154 also has an elevated side 172 and an  
7 elevated side 174. Additionally, the adapter frame 154 also contains the vertical adapter rods 176,  
8 178, 180, 182. The vertical adapter rods 176-182 are configured to engage the injector head. One  
9 of the advantages is that the adapter frame 154 can be differently sized to fit with various injector  
10 head sizes. In other words, the adapter frame 154 may be customized as being larger or smaller in  
11 order to accommodate a specific sized injector head.

12 Referring now to Fig. 2, an isometric assembled view of the apparatus 2 of the preferred  
13 embodiment seen in Fig. 1 will now be described. The z-axis frame 62 is pivotally attached to the x-  
14 axis frame 26 via the pin 74. The cylinder 42 has the piston 43 extending therefrom, and the piston  
15 is connected to bracket 79. As noted earlier, a second cylinder and piston (not shown in this view)  
16 will be connected on the opposite side in a similar manner. The cylinder 42 and piston 43 are part  
17 of the motion restriction system that will be explained in greater detail later in the application. The  
18 z-axis frame 62 can therefore be pivoted as shown by arrow B. The x-axis frame 26 can also be  
19 pivoted via the bushings 48, 52 (48, 52 not shown in this figure), as shown by arrow A.

20 Additionally, Fig. 2 depicts the vertical rods 110, 112, 114, and 116 extending through the  
21 openings 142, 144, 146, and 148, respectively. In this manner, the sliding pad 102 can slid on the  
22 cover plate 80 (as seen in Figs. 1A and 1B), and the sliding frame assembly 92 (as seen in Fig. 1B)

1 can move laterally a distance equal to the diameter of the openings 142, 144, 146, 148 in all  
2 directions. Fig. 2 further depicts the vertical adapter rods 176-182 that will be connected to the  
3 injector head. In this way, the adapter frame 154 will be connected to the injector head, and the  
4 injector head will be connected to the riser. Hence, the movement of the platform relative to the  
5 riser is compensated by the apparatus 2 herein disclosed.

6 In Fig. 3, a cross-sectional view of the isometric illustration of the apparatus 2 taken along  
7 line 3-3 of Fig. 2 will now be described. The x-axis frame 26 is shown being connected to the base  
8 frame 4 wherein the cylinder 16 has the piston 56 that is connected to the side 30 of the x-axis  
9 frame 26 and the cylinder 18 has the piston 58 that is also connected to the side 34 of the x-axis  
10 frame 26. In the preferred embodiment shown in Fig. 3, the sides of the various frames are  
11 constructed of square tubular members.

12 The z-axis frame 62 has the pin 74 disposed through the side 66 of the z-axis frame 62 as  
13 well as the pin 186 disposed through the side 188 of the z-axis frame 62 so that the z-axis frame is  
14 pivotal as shown by the arrow B. Also, the cover plate 80 is shown.

15 Fig. 3 also depicts the top plate weldment 140 being attached via nuts and bolts, such as  
16 seen at 189. As noted earlier, the top plate weldment 140 is attached to the lip structure 84. As  
17 seen in Fig. 3, the top plate weldment 140 and the cover plate 80 form a cavity C that contains the  
18 sliding frame assembly 92. Note that the second strip elastomer 104 rest on the cover plate 80,  
19 however, the first strip elastomer 102 will not engage the top plate weldment 140 so that the  
20 sliding frame assembly 92 can laterally move within this cavity. The lateral movement will be  
21 limited by the diameter of the openings through the top plate weldment 140, for instance openings  
22 142 and 148 seen in Fig. 3. The movement is limited since the vertical rods of the sliding frame

1 assembly 92 are disposed through the openings, such as the vertical rod 110 and 116 seen in Fig. 3.

2 Fig. 3 also depicts the locking means for locking and indexing the sliding frame assembly  
3 92, wherein the rods 126 and 130 are shown. The rods can be advanced through an opening in the  
4 sides of the z-axis frame via thread means. The rods will push the sliding frame assembly 92 and in  
5 this way, the sliding frame assembly 92 can be locked into place; also, the operator may use the  
6 locking means to index the sliding frame assembly into a known position within the cavity C.

7 The adapter frame 154 is shown in engagement with the vertical rods 110, 116 of the  
8 sliding frame assembly 92. As seen in Fig. 3, the vertical rod 110 is disposed through the opening  
9 164 and the vertical rod 116 is disposed through the opening 170. As noted earlier, the adapter  
10 rods will connect to the base of a coiled tubing injector head in the preferred embodiment.

11 Referring now to Fig. 4, a schematic illustration of the apparatus 2 of the most preferred  
12 embodiment of the present invention as part of the well intervention string assembly on a floating  
13 platform, such as a semi-submersible drilling rig, will now be described. Fig. 4 depicts a motion  
14 compensation means 200 that is attached to a floating platform 202. The motion compensation  
15 system 200 was described in a patent application filed by applicant on 15 December 2003 entitled  
16 “Motion Compensation System and Method”, bearing serial number 10/736,267, which is  
17 incorporated herein by reference. The motion compensation system is operatively connected to a  
18 track stack structure 203. The track stack structure 203 is commercially available from Devin  
19 International Inc. under the name Track Stack Jr. (hereinafter referred to as a track stack). The  
20 apparatus 2 is attached to the track stack structure 203. The purpose of the track stack is to allow  
21 movement of a supporting platform in a vertical plane as well as a horizontal plane.

22 The floating platform 202 will be tethered to the ocean floor 204 via conventional means

1 such as anchors. A riser 206 extends from the ocean floor 204 to the platform 202. The riser 206  
2 is connected at one end to the subterranean well 208, and at the other end to the coiled tubing  
3 injector head 210. The coiled tubing injector head 210 is commercially available from Hydra Rig  
4 Corporation under the name Coiled Tubing Injector Head. The adapter frame 154 is connected to  
5 the coiled tubing injector head 210. The base frame 4 is connected to the track stack 203 which is  
6 connected to the motion compensation means 200 which in turn is connected to the floating  
7 platform 202; hence, the base frame 4 is in effect attached to the floating platform 202. Fig. 4 also  
8 depicts a blow out preventor stack 212.

9 As noted earlier, the wave and tidal effects on the riser 206 and platform 202 do not occur  
10 in unison. The riser 206 and the coiled tubing injector head 210 will be held static for the most  
11 part since the riser 206 is connected to the subterranean well 208, while the floating platform 202  
12 and attached base frame 4 will experience various buoyant forces thereby causing the base frame 4  
13 to undergo heave, pitch and yawl, as understood by those of ordinary skill in the art. In the view  
14 of Fig. 4, the coiled tubing injector head 210 is still in a vertical orientation relative to the platform,  
15 and therefore, there is no tilting and/or pivoting in the apparatus 2.

16 In Fig. 5, a schematic illustration of the apparatus 2 seen in Fig. 4 with a tilt angle "T1" of  
17 approximately 2 degrees to the port side is shown. Hence, in this sequence, the x-axis frame 26  
18 has pivoted on the cradles 36, 38 (not shown in this view). Note that the cylinders 42, 44 (not  
19 shown in this view) act as a biasing means and prevents over rotation of the x-axis frame 26. Fig.  
20 6 depicts the schematic illustration of the apparatus 2 seen in Figs. 4 and 5, wherein the tilt angle  
21 of approximately 2 degrees "T2" is to the starboard side. As seen in Fig. 6, the x-axis frame 26 has  
22 pivoted on the cradles 36, 38 (not shown in this view).

1 Referring now to Fig. 7, a schematic illustration of the top view of the apparatus 2 seen in  
2 Fig. 4 will now be discussed. The coiled tubing injector head 210 is attached to the adapter frame  
3 154. Note that rods 112, 114, 116, and 118 are disposed concentrically through the openings 142,  
4 144, 146, 148, respectively. In this view, the apparatus 2 is essentially centered.

5 Fig. 8 is a schematic illustration of the top view of the apparatus 2 seen in Fig. 7 depicting  
6 lateral travel. Thus, the motion of the entire well intervention string assembly and the platform 202  
7 has caused lateral motion. Fig. 8 depicts the amount of lateral motion, represented by the arrow  
8 "D". In the preferred embodiment, the openings are 18 inches in diameter; therefore, there is a  
9 maximum travel of 9 inches in any one plane.

10 Fig. 9 is a schematic illustration of the motion compensation system 220 of the present  
11 invention which is also referred to as the motion restriction system. The motion compensation  
12 system 220 includes biasing means for biasing the x-axis frame 26, and wherein x-axis biasing  
13 means includes the cylinder 16 and the cylinder 18. The system 220 also includes biasing means  
14 for biasing the z-axis frame 62, and wherein the z-axis biasing means includes the cylinder 42 and  
15 cylinder 44. In the preferred embodiment, the cylinders will be powered via a hydraulic source  
16 222. The cylinders 16, 18, 42, 44 serve to limit the pivoting movement of the relative frame, as  
17 well as providing a resistance to the pivoting movement. It should be noted that other biasing  
18 means could be provided. For instance, the cylinders could contain springs, and wherein the  
19 springs would both limit the pivoting range, as well as providing resistance to the pivoting motion.  
20 In the most preferred embodiment, a hydraulic system that has a nitrogen pressure source 228, 230  
21 for maintaining the hydraulic fluid of the hydraulic system under pressure will be used as shown in  
22 Fig. 9.

1           The x-axis biasing means can be described as follows with reference to Fig. 9. The  
2       hydraulic supply 222 will be directed to valves 232, 234, then to the cylinders 18, 16. Valve means  
3       232, 234 will allow the hydraulic fluid to the cylinders 16, 18 as shown. The nitrogen supply 228,  
4       which is pressurized nitrogen gas, is directed to the accumulators 236 and 238. Note that valves  
5       232, 234 are in communication with accumulators 236, 238, and wherein the accumulators 236,  
6       238 provide for additional volume and storage of the nitrogen gas in order to keep the system with  
7       the proper pressure. Thus, the x-axis biasing means can bias the x-axis frame 26 along the x-axis  
8       utilizing the pressurized hydraulic system shown.

9           The z-axis biasing means will now be described. The hydraulic supply 222 will be directed  
10      to valves 240, 242, then to the cylinders 42, 44. Valve means 240, 242 will allow the hydraulic  
11      fluid to the cylinders 42, 44 as shown. The nitrogen supply 230 is directed to the accumulators  
12      244, 246. The valves 240, 242 are in communication with accumulators 236, 238, and wherein the  
13      accumulators 244, 246 provide for additional volume and storage of the nitrogen gas in order to  
14      keep the system pressurized. Hence, the z-axis biasing means can bias the z-axis frame 62 along  
15      the z-axis utilizing the pressurized hydraulic system shown.

16           Although the present invention has been described in terms of specific embodiments, it is  
17      anticipated that alterations and modifications thereof will no doubt become apparent to those  
18      skilled in the art. It is therefore intended that the following claims be interpreted as covering all  
19      such alterations and modifications as fall within the true spirit and scope of the invention.